

# Data processing description

Bruno Piguet

EUFAR/TETRAD, 10-17 September 2010

# Introduction

Processed Data

B. Piguet

Introduction

Positionning

Pressure

Relative wind

Temperature

Humidity

Dew point

Relative

Absolute

wind

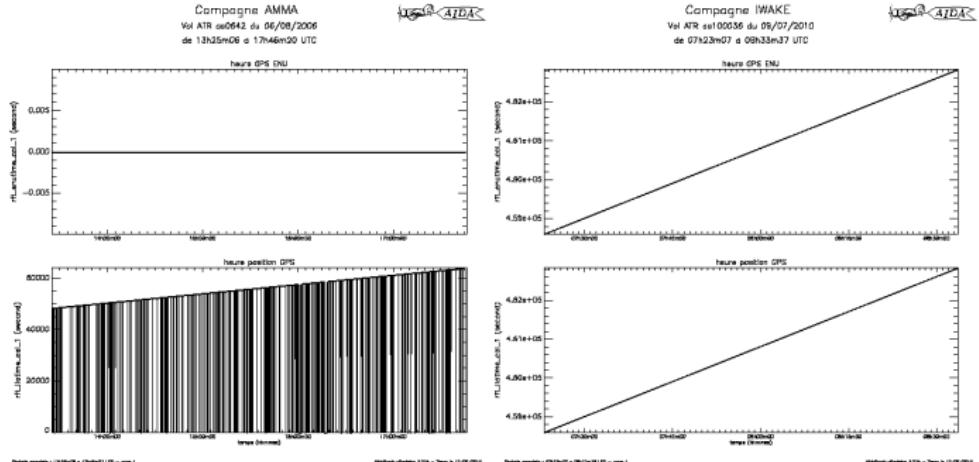
LWC

radiation

What happened between the sensor and the file you get ?

# Processing : nothing scientific

## What to check : data loss



Introduction

Positionning

Pressure

Relative wind

Temperature

Humidity

Dew point

Relative

Absolute

wind

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Introduction

Positionning

Pressure

Relative wind

Temperature

Humidity

Dew point

Relative

Absolute

wind

LWC

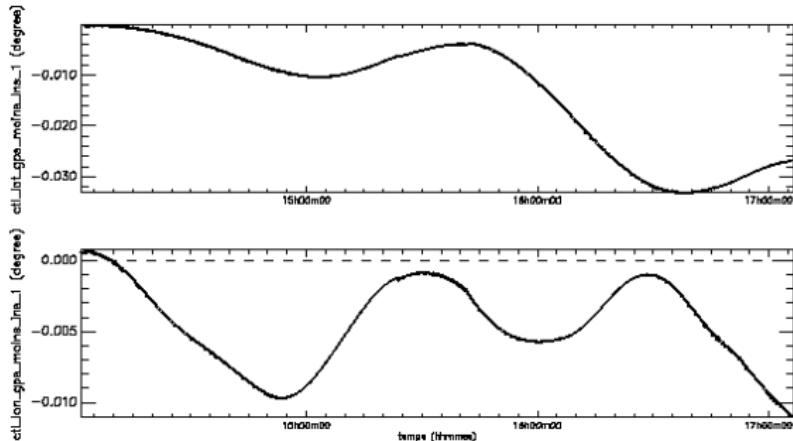
radiation

# INS, for positions

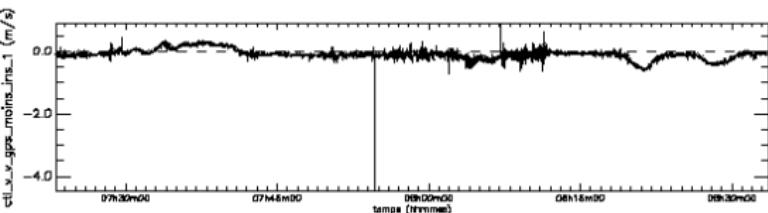
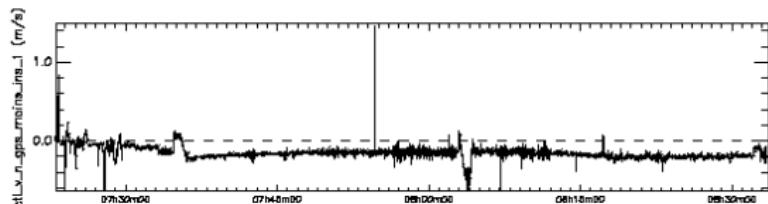
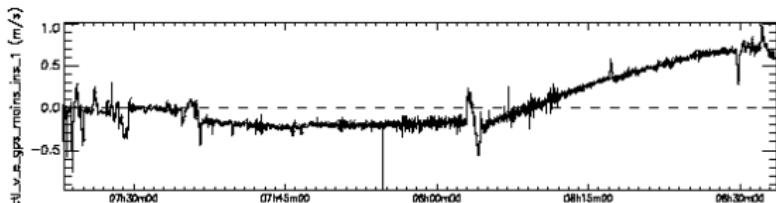
Processing : nothing scientific

What to check : Drift, Schuler oscillation.

Campagne EYJAFJOLL  
Vol ATR 0010019 du 12/05/2010  
de 14h01m36 à 17h06m27 UTC



Campagne IWAKE  
Vol ATR ee100036 du 09/07/2010  
de 07h23m07 à 08h33m37 UTC



Introduction

Positionning

Pressure

Relative wind

Temperature

Humidity

Dew point

Relative

Absolute

wind

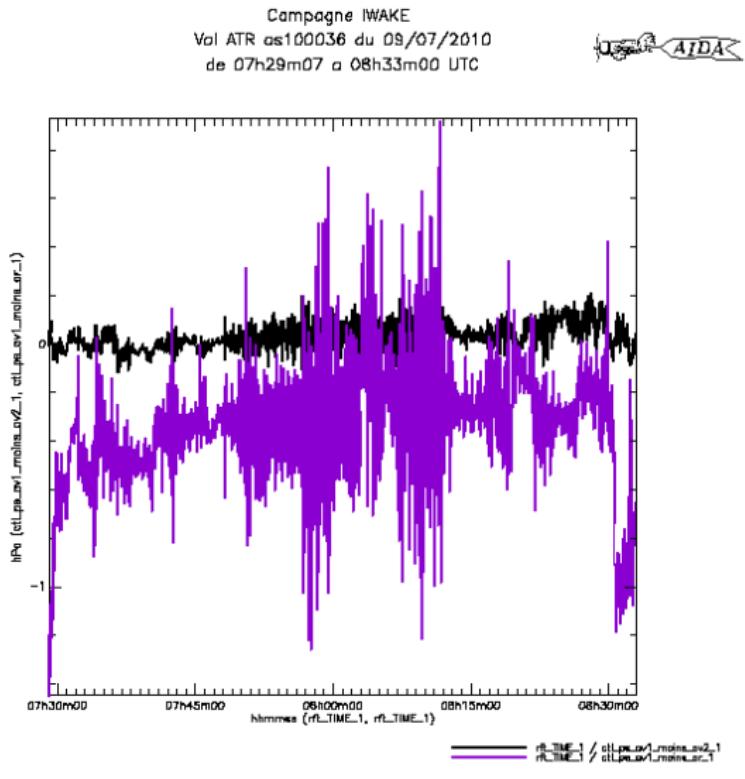
LWC

radiation

# Pressure

Processing : "static defect" removal

What to check : similarity of redundant measurements.



Introduction

Positionning

Pressure

Relative wind

Temperature

Humidity

Dew point

Relative

Absolute

wind

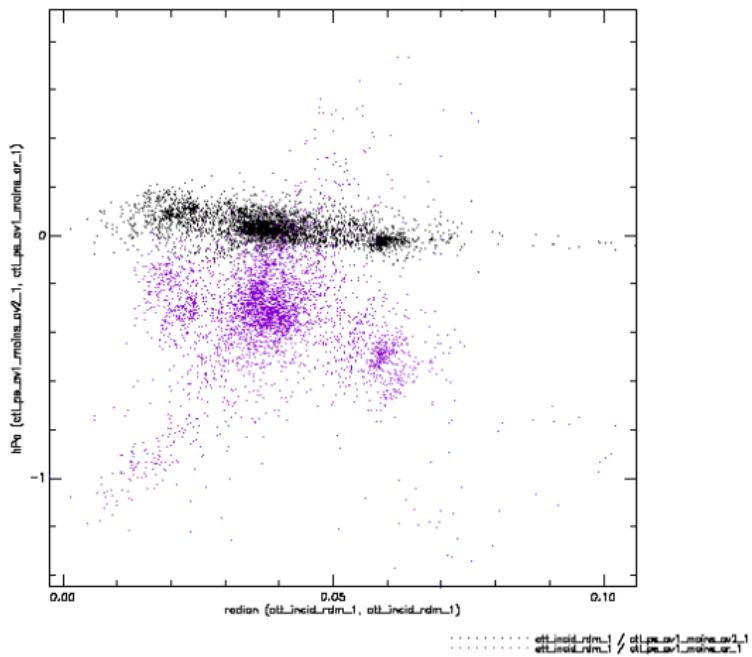
LWC

radiation

# Pressure (2)

Looking for a correlation of the error to a cause.

Campagne WAKE  
Vol ATR as100036 du 09/07/2010  
de 07h29m07 à 08h33m00 UTC



Introduction

Positionning

Pressure

Relative wind

Temperature

Humidity

Dew point

Relative

Absolute

wind

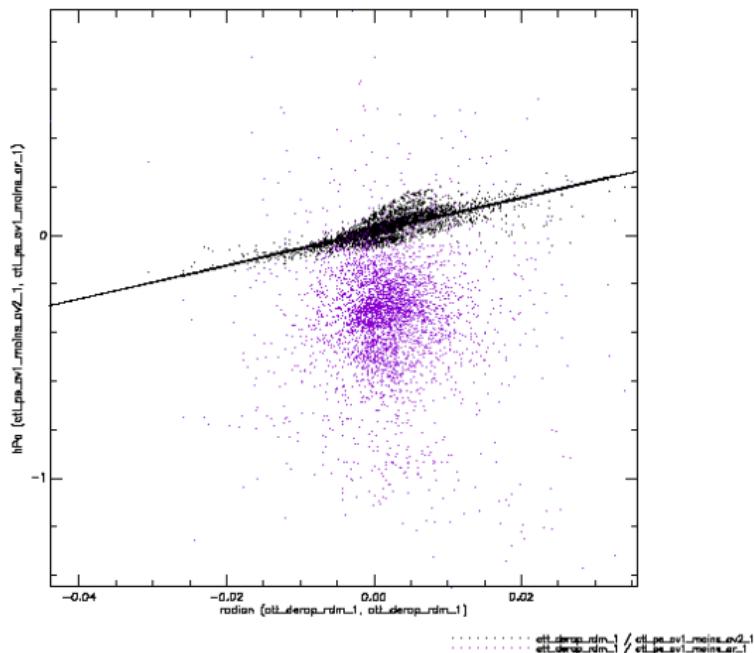
LWC

radiation

# Pressure (3)

Looking for a correlation of the error to a cause.

Campagne IWAKE  
Vol ATR as100036 du 09/07/2010  
de 07h29m07 à 08h33m00 UTC



Regression linéaire :  $Y = 8.87885X + 0.0204981$ , corrélation : 0.768477

Aerosol Retrieval IWAKE - Trace le 12/03/2010

Introduction

Positionning

Pressure

Relative wind

Temperature

Humidity

Dew point

Relative

Absolute

wind

LWC

radiation

[Introduction](#)[Positionning](#)[Pressure](#)[Relative wind](#)[Temperature](#)[Humidity](#)[Dew point](#)[Relative](#)[Absolute](#)[wind](#)[LWC](#)[radiation](#)

# Air speed

Processing : "static defect" removal, then pressure to speed conversion :

$$V_p^2 = 2 \cdot c_{pa} \cdot T_s \cdot \left[ \left( 1 + \frac{\Delta P}{P_s} \right)^{R_a/c_{pa}} - 1 \right]$$

What to check : similarity of redundant measurements.

# Air flow direction

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Introduction

Positionning

Pressure

Relative wind

Temperature

Humidity

Dew point

Relative

Absolute

wind

LWC

radiation

Processing : Conversion of differential pressure to angle (*cf.* theory and calibration)

$$\alpha = \alpha_0 + k \frac{\Delta P}{\Delta P} - \alpha$$

For a Rosemount 858,  $k = 12.8$  (in degrees).

What to check : Icing

# A simple qualitative radôme icing test

Processed Data

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Introduction

Positionning

Pressure

Relative wind

Temperature

Humidity

Dew point

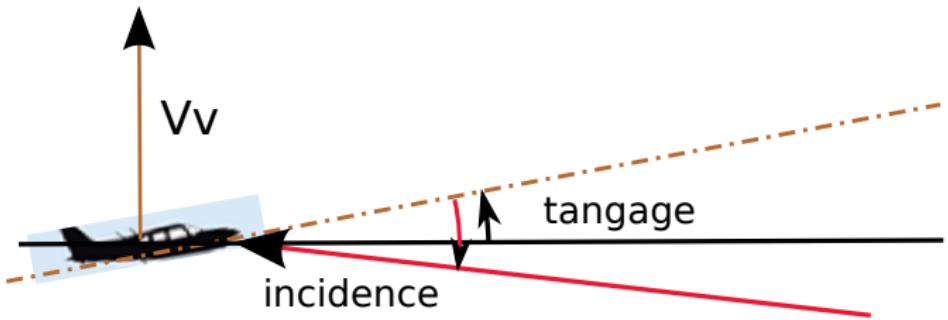
Relative

Absolute

wind

LWC

radiation



If  $\omega \ll Vv$ ,  $(pitch - attack) * Vp \approx Vv$

$Vv$  can come from various sources : INS, GPS,  $dP/dt$

Most of the time, discrepancy comes from *attack*

Introduction

Positionning

Pressure

Relative wind

Temperature

Humidity

Dew point

Relative

Absolute

wind

LWC

radiation

# Temperature

Processing :

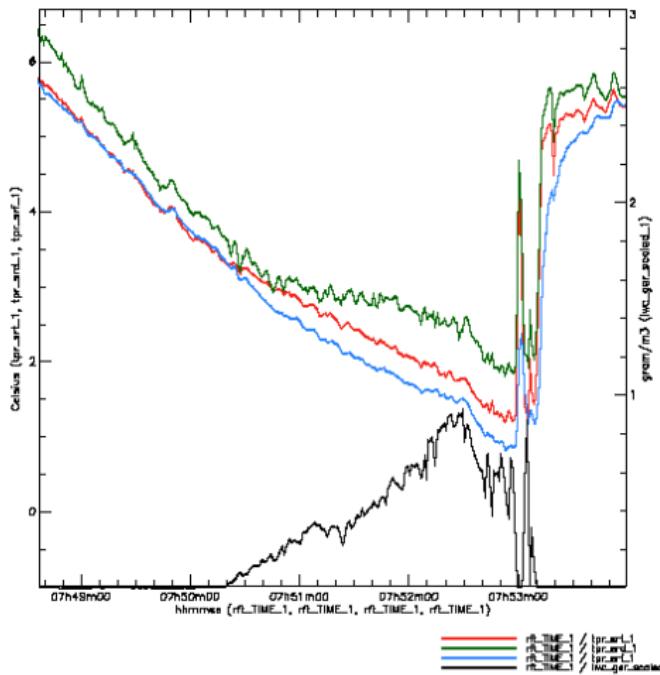
$$T_s = \frac{T_t}{1 + r_f \times \left( \left( 1 + \frac{\Delta P}{P_s} \right)^{R_a/c_{pa}} - 1 \right)}$$

What to check : similarity of redundant measurements.

Series of differences, correlation of differences to a plausible cause.

# Temperature - comparison

Campagne EUCAARI  
 Vol ATR as0851 du 15/05/2008  
 de 07h48m37 à 07h54m00 UTC



Introduction

Positionning

Pressure

Relative wind

Temperature

Humidity

Dew point

Relative

Absolute

wind

LWC

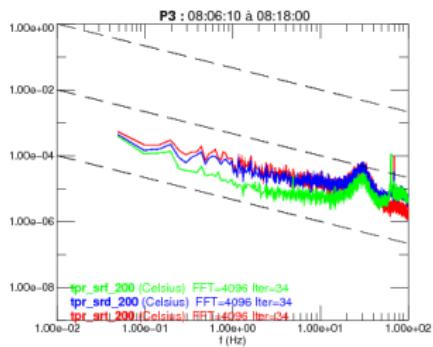
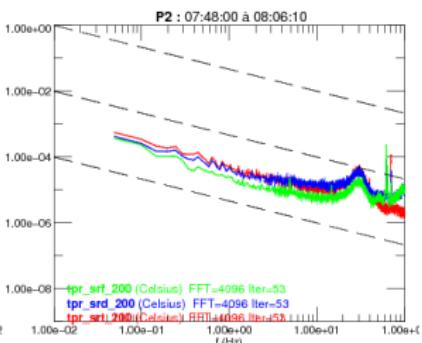
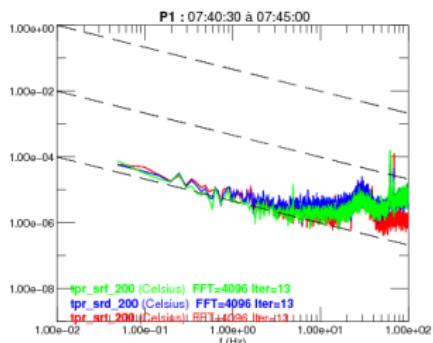
radiation

# Temperature - spectra

Densité Spectrale de Puissance \* Freq

iwake

Acquisition : as100036 du 09/07/2010



Introduction

Positionning

Pressure

Relative wind

Temperature

Humidity

Dew point

Relative

Absolute

wind

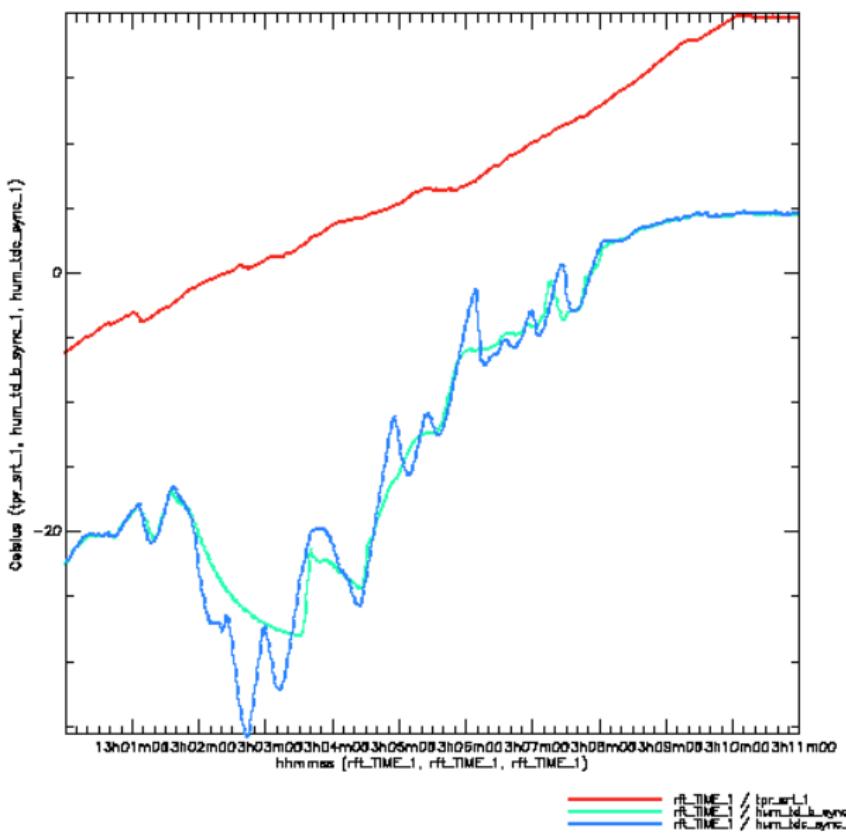
LWC

radiation

Campagne TETRAD  
ATR42 as100050 du 10/09/2010  
de 13h00m00 à 13h11m00 UTC

Processed Data

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Introduction

Positionning

Pressure

Relative wind

Temperature

Humidity

Dew point

Relative

Absolute

wind

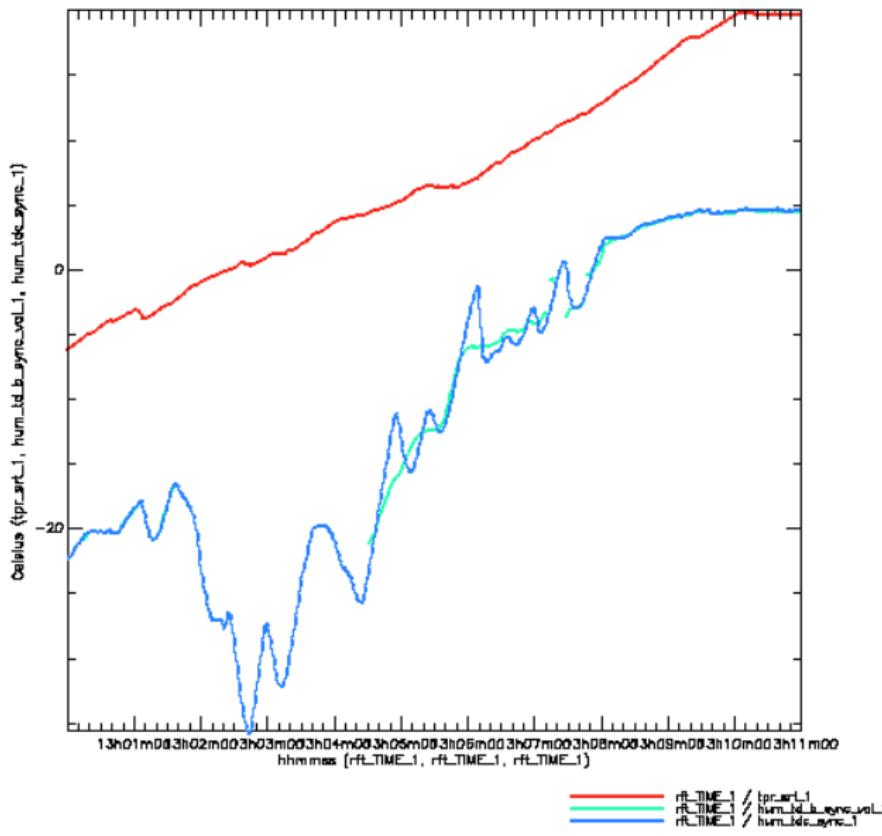
LWC

radiation

Campagne TETRAD  
ATR42 as100050 du 10/09/2010  
de 13h00m00 à 13h11m00 UTC

Processed Data

B. Piguet



Introduction

Positionning

Pressure

Relative wind

Temperature

Humidity

Dew point

Relative

Absolute

wind

LWC

radiation

# Capacitive probe : relative humidity sensor

Processed Data

B. Piguet

Introduction

Positionning

Pressure

Relative wind

Temperature

Humidity

Dew point

Relative

Absolute

wind

LWC

radiation

Processing :

Correction of the two effects of fast air flow stopping on the sensor : change of pressure and temperature.

Empirical calibration with a reference computed from dew point hygrometers.

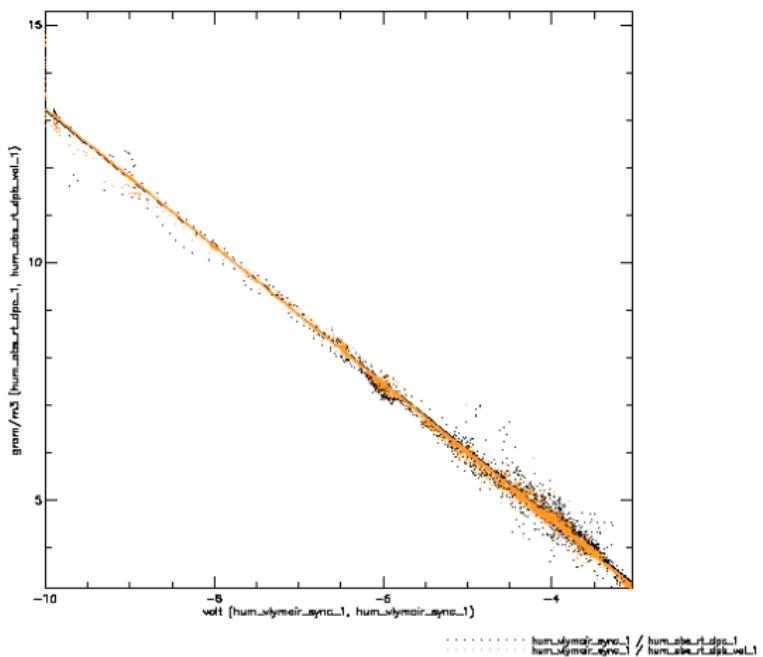
What to check : aging, change of behaviour after wetting.

# Lyman- $\alpha$ : Absolute humidity sensor

Processed Data

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Campagne IWAKE  
Vol ATR as100036 du 09/07/2010  
de 07h32m00 à 08h29m00 UTC



Introduction

Positionning

Pressure

Relative wind

Temperature

Humidity

Dew point

Relative

Absolute

wind

LWC

radiation

# Wind - computation (1)

If the velocity of the aircraft with respect to ground, is expressed in the aircraft frame :

Velocities sum in the aircraft frame :

$$\mathbf{V}_{air/ground} = \mathbf{V}_{air/rad} + \boldsymbol{\Omega}_{(av/ground)} \wedge \mathbf{X}_{rad} + \mathbf{V}_{aircraft/ground}$$

Rotation to the local geographic frame :

$$\text{Wind} = \mathbf{V}_{air/ground(\text{geo})} = [\mathbf{M}_{\text{att}}] [\mathbf{V}_{air/ground(\text{aircraft})}]$$

Where :

$\mathbf{X}_{rad}$  : coordinates of the radome in the frame of the velocity measurement system

$[\mathbf{M}_{\text{att}}]$  : rotation matrix corresponding to attitude angles.

## Wind - computation (2)

If the velocity of the aircraft with respect to ground is expressed in the geographic frame :

Computation of  $V_{air/aircraft}$  at the location of velocity measurements, in the aircraft frame

$$V_{air/aircraft} = V_{air/rad} + \Omega_{(av/ground)} \wedge X_{rad}$$

Rotation to the local geographic frame :

$$V_{air/aircraft(geo)} = [M_{att}] [V_{air/aircraft(aircraft)}]$$

Simple sum at the end, in the local geographic frame :

$$\text{Wind} = V_{air/aircraft} + V_{aircraft/ground}$$

[Introduction](#)[Positionning](#)[Pressure](#)[Relative wind](#)[Temperature](#)[Humidity](#)[Dew point](#)[Relative](#)[Absolute](#)[wind](#)[LWC](#)[radiation](#)

# Statistical empirical corrections

Under the hypothesis of uniform wind, two back-and-forth legs allow to compute biases.

This can be generalized to any angle (Maurel 1995), and it gives you a statistics of corrective terms along a campaign.

Processing :

$$LWC = \frac{P_w - A(T_w - T_s).(\rho \cdot V_p)^\chi}{l.d.V_p.[L + c.(T_{wh} - T_s)]}$$

where  $L = 2.264 \cdot 10^6 \text{ J.kg}^{-1}$  (Water latent heat at  $100^\circ\text{C}$ )  
and  $c = 4218 \text{ J.kg}^{-1}$  (Specific water heat)

What to check :

- ▶ Dry air term.
- ▶ Physical plausibility (compare to adiabatic vertical profile)

Introduction

Positionning

Pressure

Relative wind

Temperature

Humidity

Dew point

Relative

Absolute

wind

LWC

radiation

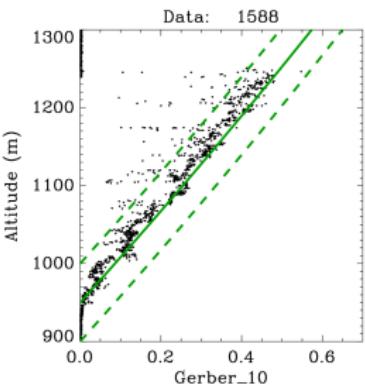
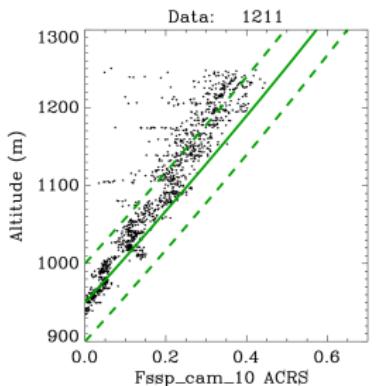
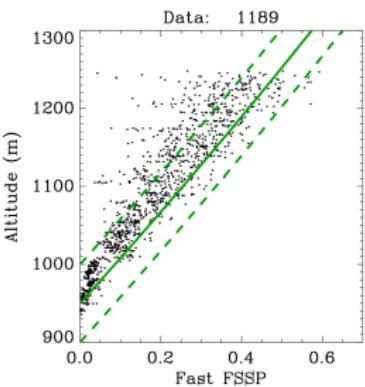
EUCAARI as0852 – at0809

## VERTICAL PROFILES

of LWC ( $\text{g} \cdot \text{m}^{-3}$ )

at: 114950.3

Base parameters:

 $Z = 950.$  (m) $P = 908.0$  (hPa) $T = 2.3$  (C)

Introduction

Positionning

Pressure

Relative wind

Temperature

Humidity

Dew point

Relative

Absolute

wind

LWC

radiation

Introduction

Positionning

Pressure

Relative wind

Temperature

Humidity

Dew point

Relative

Absolute

wind

LWC

radiation

# radiation

Processing :

Long-wave thermal equilibrium :

$$Flx = a \cdot V_{th} + \sigma \cdot T_b^4 + K \cdot \sigma \cdot (T_b^4 - T_c^4)$$

Short-wave :

We **don't** do any attitude correction.

What to check :

comparisons to :

- ▶ other measurements
- ▶ physically plausible estimates

# Comparaison to sea temperature

Processed Data

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Introduction

Positionning

Pressure

Relative wind

Temperature

Humidity

Dew point

Relative

Absolute

wind

LWC

radiation

